

# Standard Library Plant Controller Model Specification for a Grid-Forming Hybrid Control Inverter-based Resource (REPCGFM\_C1)

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# **1** Introduction

This document describes a standard library plant controller model to interface with the gridforming hybrid control inverter-based resource (IBR) model. The initial version of model specification was jointly developed by Pacific Northwest National Laboratory (PNNL), Tesla Energy, and EPRI, and it was revised multiple times later to incorporate suggestions from WECC MVS members. Tesla Energy provided main control blocks to support the development of this model specification.

This standard library model is developed to help the utility industry better understand the GFM technology. The model could be used to represent equipment for long-term planning studies where vendor-specific models are not available. As equipment mature and improve, standard library models will be updated to capture the new functionalities of GFMs. It is not intended that these models will always remain representative of all future GFM technologies.

# 2 Overall Control Structure

Figure 1 shows the overall control structure of the plant controller. It sends the active and reactive power references to the GFL branch and the voltage and frequency references to the GFM branch of the GFM hybrid IBR model.



Figure 1 Overall control structure.

# **3** Voltage and Frequency Reference Generator for the GFM Branch

Figure 2 and Figure 3 show the voltage and frequency reference generator for the GFM branch. In Figure 2,  $f_{site}$  refers to the frequency at the plant bus, or a remote bus.  $f_{ref}$  will be connected to  $\omega_{ref}$  in the REGFM\_C1 inverter model.



Figure 2 Frequency reference generator for the GFM branch.

In Figure 3,  $V_{site}$  refers to the voltage of the plant bus, or a remote bus. V refers to the inverter terminal voltage.  $\frac{P_{target} - jQ_{target}}{1}$  represents the current in per unit value assuming the plant bus voltage is 1 pu. Because the plant bus voltage is not always 1 pu in a real system,  $\Delta V_{err}$  is added in Figure 3 to simplify the initialization.



Figure 3 Voltage reference generator for the GFM branch.

## 4 Active and Reactive Power Blocks for the GFL Branch

Figure 4 and Figure 5 show the active and reactive power paths, and Figure 6 shows the voltage control added on the reactive power path.



Figure 4 Active power path for the GFL branch.

In Figure 4, the calculation of  $\Delta P_{loss}$  assumes the plant voltage is 1 pu.  $P_{site}$  refers to the plant output active power, which is the same with the branch power ( $P_{branch}$ ).

Note that the fast frequency response (FFR) function is implemented in the plant controller as shown in Figure 4. The FFR function is described as follows:

**FFR Function**: Once  $f_{site\_meas}$  drops below  $f_{FFR\_low}$  or exceeds  $f_{FFR\_high}$ , a pre-determined value  $P_{FFR\_low}$  or  $P_{FFR\_high}$  will be added on the power referee of the plant controller and lasts for a period of  $T_{FFR}$ , and after that  $P_{FFR\_low}$  or  $P_{FFR\_high}$  will gradually return to 0 with a ramp rate of  $D_{FFR}$ . Once  $P_{FFR\_low}$  or  $P_{FFR\_high}$  is added on the power reference, the FFR function will not detect  $f_{site\_meas}$ , and it will only detect whether  $f_{site\_meas}$  is below  $f_{FFR\_low}$  or above  $f_{FFR\_high}$  again after  $P_{FFR\_low}$  or  $P_{FFR\_high}$  returns to 0.

In Figure 5, the calculation of  $\Delta Q_{loss}$  assumes the plant voltage is 1 pu.  $Q_{site}$  refers to the plant output reactive power, which is the same with the branch reactive power ( $Q_{branch}$ ).



• When VFlag=1,  $Q_{Vref_site} = Q_{target} = Q_{site}$ , and  $Q_{ref_site} = 0$ 

#### Figure 5 Reactive power path for the GFL branch.

Figure 6 shows the voltage control block for the GFL branch. Note that the integral gain  $K_{i\_vc}$  can also be set as 0 so that the plant control follows the *Q*-*V* droop.



Figure 6 Voltage control block for the GFL branch.

### **Table 1 Parameters**

Name	Description	Unit	Example Value
Deep March 1	Bus number for voltage control. $V_{site}$ in the specification refers	NT A	NT A
Bus Number	to the voltage at the specified Bus Number.	NA	NA
EDOM Due	Monitored branch FROM bus number for calculating $P_{branch}$ and	NIA	NA
FROM Bus	$Q_{branch}$ . $P_{site}$ in the specification refers to $P_{branch}$ .	INA	INA
TO Due	Monitored branch TO bus number for calculating $P_{branch}$ and	NΛ	NΔ
TO Bus	$Q_{branch}$ . $Q_{site}$ in the specification refers to $Q_{branch}$ .	пл	
Circuit ID	Branch circuit ID for calculating $P_{branch}$ and $Q_{branch}$	NA	NA
VFlag	A flag to determine if the voltage control for the GFL branch is	NA	1
villag	enabled (1) or disabled (0).	1111	1
	A flag to select whether the plant voltage measurement (1) or		
$V_{ref}$ Flag	the inverter voltage measurement (0) is used to generate the	NA	1
	voltage reference of the GFM branch.		
FFRFlag	A flag to select whether the FFR function is enabled (1) or	NA	0
1110.008	disabled (0).		, , , , , , , , , , , , , , , , , , ,
frefmax	Upper limit of the frequency reference generator of the GFM	pu	1.05
<i>J</i> reginal	branch.	1	
frefmin	Lower limit of the frequency reference generator of the GFM	pu	0.95
j rejnan	branch.	r -	0,50
frmax	Upper rate limiter for the plant frequency measurement	pu/s	0.05
frmin	Lower rate limiter for the plant frequency measurement	pu/s	-0.05
V <sub>fth</sub>	Voltage threshold for the plant frequency measurement	pu	0
$T_{frq}$	Time constant of the low-pass filter.	S	0.02
T <sub>fref</sub>	Time constant of the low-pass filter.	S	0.3
Rloss	Resistance used to estimate the active power loss of the plant.	pu	Resistance of the
			transformers
$X_{loss}$	Reactance used to estimate the reactive power loss of the plant.	pu	Reactance of the
1055		P	transformers
Vrefmax	Upper limit of the voltage reference generator of the GFM	pu	1.1
	branch.	1	
V <sub>refmin</sub>	Lower limit of the voltage reference generator of the GFM	pu	0.85
T	branch.		0.01
I Vmeas	Time constant of the low-pass filter for voltage measurement.	S	0.01
I Vref	Time constant of the low-pass filter.	S	0.3
T <sub>Vlag</sub>	Emulate the time delay of sending the inverter terminal voltage	S	0.2
dh	I ower threshold of the frequency deadhand		0.0005
$\frac{dD_{fL1}}{dh}$	Lower threshold of the frequency deadband	pu	-0.0005
D	Depundide of frequency versus newer droop gain	pu	0.0003
$D_{dn}$	Unside of frequency versus power droop gain	pu	20
$D_{up}$	Upper limit of the frequency versus power droop gain	pu	20
P <sub>freq_max</sub>	reference	pu	2
	Lower limit of the frequency versus active power droop		
$P_{freq\_min}$	reference	pu	-2
Pc	Unper limit of the active power reference	nu	0.95
Prof. reit	Lower limit of the active power reference	nu	_0.95
T ref_min	Time constant of the low-pass filter for P measurement	e pu	0.00
<i>K</i> .	Controller gain for the active power path	5 DU	0.01
<b>P</b>	Unper limit of the integrator for the active power path	pu nu	0.1
P .	Lower limit of the integrator for the active power path	pu nu	0.1
▲ err_min			
Parman	Upper limit of the input for the active power path	nu	0.1
Perr_rmax Perr_rmin	Upper limit of the input for the active power path Lower limit of the input for the active power path	pu pu pu	-0.1 -0.1

T <sub>Plag</sub>	Emulate the time delay of sending the <i>P</i> command from the plant controller to the inverter controller	s	0.04
$Q_{ref\_max}$	Upper limit of the reactive power reference	pu	0.3122
$Q_{ref\_min}$	Lower limit of the reactive power reference	pu	-0.3122
T <sub>Qmeas</sub>	Time constant of the low-pass filter for <i>Q</i> measurement.	s	0.01
K <sub>iq</sub>	Controller gain for the reactive power path	pu	0.1
Qerr_max	Upper limit of the integrator for the reactive power path	pu	0.1
$Q_{err\_min}$	Lower limit of the integrator for the reactive power path	pu	-0.1
Qerr_rmax	Upper limit of the input for the reactive power path	pu	0.1
$Q_{err\_rmin}$	Lower limit of the input for the reactive power path	pu	-0.1
$T_{Qlag}$	Emulate the time delay of sending the $Q$ command from the plant controller to the inverter controller	s	0.04
Verr_max	Upper limit of the voltage reference	pu	0.05
Verr_min	Lower limit of the voltage reference	pu	-0.05
$db_{VSL1}$	Lower threshold of the plant voltage controller deadband	pu	0
db <sub>VSH1</sub>	Upper threshold of the plant voltage controller deadband	pu	0
$K_{p\_vc}$	Controller gain of the plant voltage controller	pu	2
$Q_{vc\_max}$	Upper limit of the reactive power of the plant controller	pu	0.3122
$Q_{vc\_min}$	Lower limit of the reactive power of the plant controller	pu	-0.3122
$T_{vc}$	Time constant of the low-pass filter	s	0
$K_{i\_vc}$	Controller gain of the plant voltage control	pu	6
fffr_low	Lower threshold of the FFR function	pu	0.99
$f_{FFR\_high}$	Upper threshold of the FFR function	pu	1.01
P <sub>FFR_low</sub>	Power command of FFR when frequency is lower than <i>f</i> <sub>FFR_low</sub>	pu	0.3
P <sub>FFR_high</sub>	Power command of FFR when frequency is higher than <i>f</i> <sub>FFR_high</sub>	pu	-0.3
D <sub>FFR</sub>	Ramp rate for the FFR to quit operation	pu/s	0.01 pu/s
$T_{FFR}$	Time duration of the FFR	S	300

# References

[1] Sai Gopal Vennelaganti, Mostafa Mahfouz. Tesla Plant Controller Block Diagrams (Unpublished).



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