

Transient Stability Model of a Series Capacitor Metal Oxide Varistor (SCMOV)



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Reference for SCMOV Model

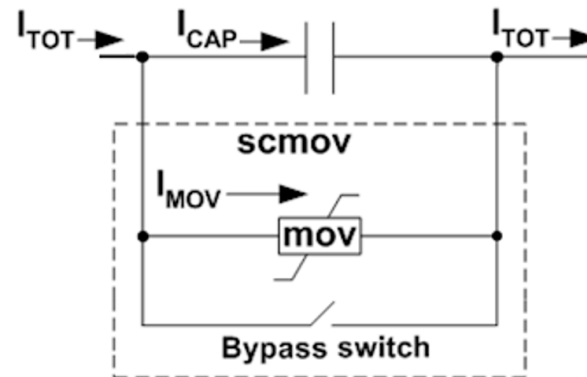


- SCMOV stands for Series Capacitor Metal Oxide Varistor (MOV)
- This model combines a set of protection equipment for over-current protection on a series capacitor
 - MOV is a device with a highly nonlinear impedance
 - At small voltage differences, the MOV exhibits very high impedance
 - As the voltage difference increases the impedance of the MOV drops quickly
 - Placing an MOV in parallel with a Series Capacitor will protect the Series Cap
 - As current on Capacitor increases, voltage drop across series cap increases → The MOV in parallel will thus have its impedance drop which pushes more of the current to the MOV
 - A bypass switch is also coupled with this MOV/Cap pair so that if the current gets high enough the bypass switch will short out both the MOV and Cap thus protecting both MOV and Capacitor

Goldsworthy Paper from 1987



- D. L. Goldsworthy, “A linearized model for MOV-protected series capacitors”, IEEE Transactions on Power Systems, Vol. PWRS-2, No. 4, November 1987
 - Describes a model that has transitions between 3 operating modes
 - NORMAL (Mode 0):
use the $R_{cap} + jX_{cap}$ from the power flow case
 - CAP+MOV (Mode 1): use a special $R_{pc} + jX_{pc}$ curve empirically determined and presented in the 1987 paper
 - BYPASS (Mode 2): Assume the bypass switch has operated and treat as a near zero impedance



Mode 0 (NORMAL)	$I_{TOT} \rightarrow R_{cap} + jX_{cap}$
Mode 1 (CAP+MOV)	$I_{TOT} \rightarrow R_{pc} + jX_{pc}$
Mode 2 (BYPASS)	$I_{TOT} \rightarrow 0 + j0.00001$

Empirically Derived Impedance



- When the MOV is conducting the Goldworthy 1987 paper found that the equivalent impedance of the CAP+MOV was consistently a multiple function of the nominal series Reactance we will call Xcap (Figure 6 in the paper on page 956)
- The paper empirically curve fits this function as follows

$$I_{pux} = \frac{I_{totAmps}}{I_{cappro} I_{crated}}$$

Restrict I_{pux} to between 0.94879 and 17.5684
to prevent MultR and MultX from being negative values

$$MultR(I_{pux}) = 0.0745 + 0.49e^{-0.243*I_{pux}} - 35.0e^{-5.0*I_{pux}} - 0.60e^{-1.4*I_{pux}}$$

$$MultX(I_{pux}) = 0.1010 - 0.005749 * I_{pux} + 2.088e^{-0.8566*I_{pux}}$$

Figure 6 from Goldsworthy 1987 Paper



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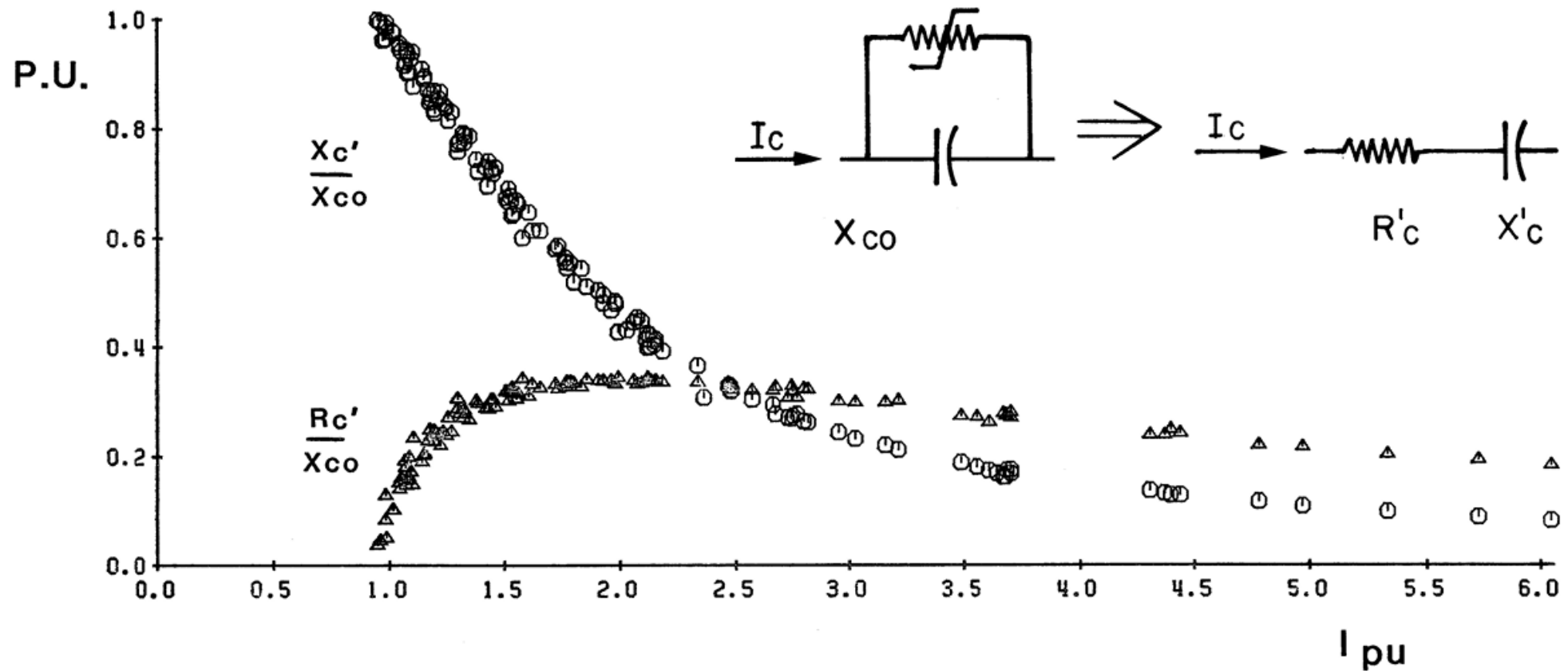
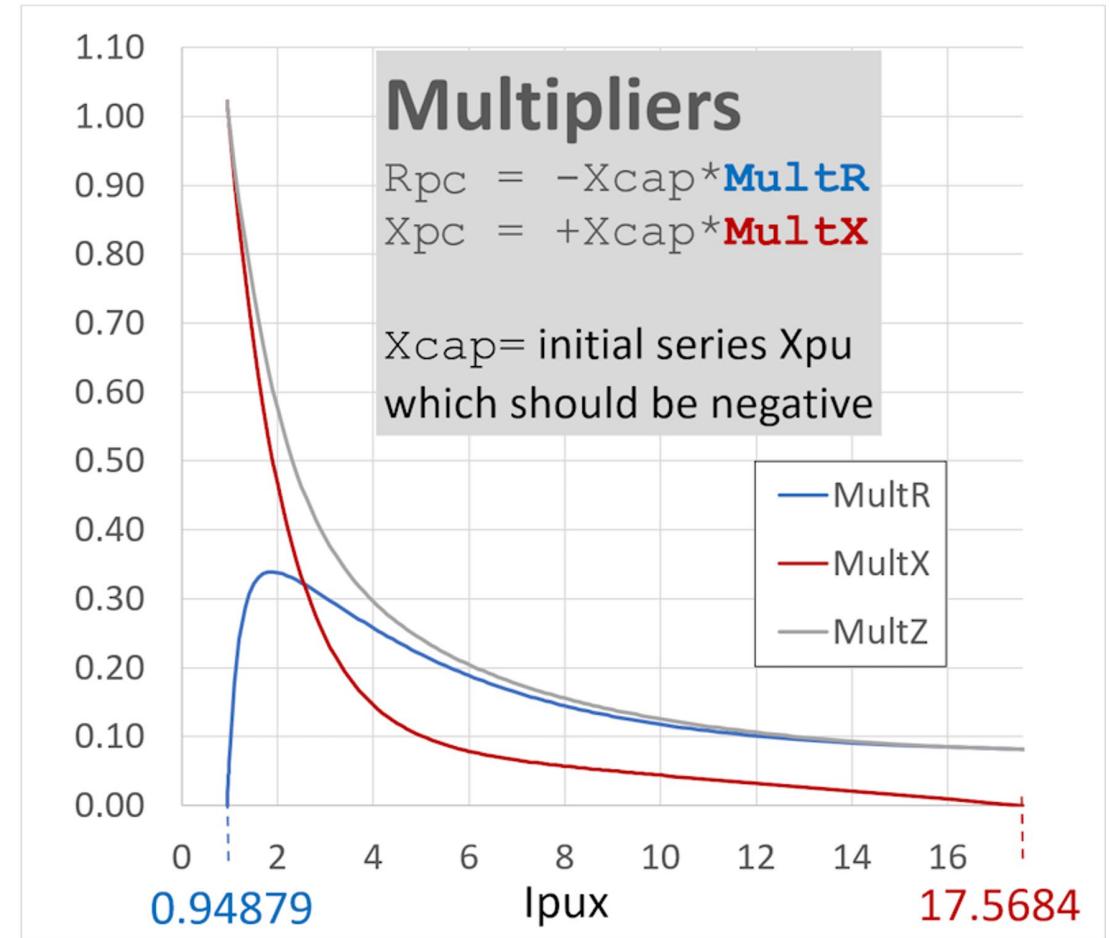


Figure 6. Normalized equivalent reactance and resistance vs. normalized current.



Graph of Multipliers

- Notice at about 0.94879
 - MultR = 0.000
 - MultX = slightly bigger than 1.000
 - (MultX = 1.000 at 0.97648)
- When calculating multipliers, we restrict I_{pux} to between 0.94879 and 17.5684
 - The empirical data is in Figure 6 of the paper only has data from 0.95 to 6.00
 - Negative multipliers do not make sense, so restrict the range to prevent them

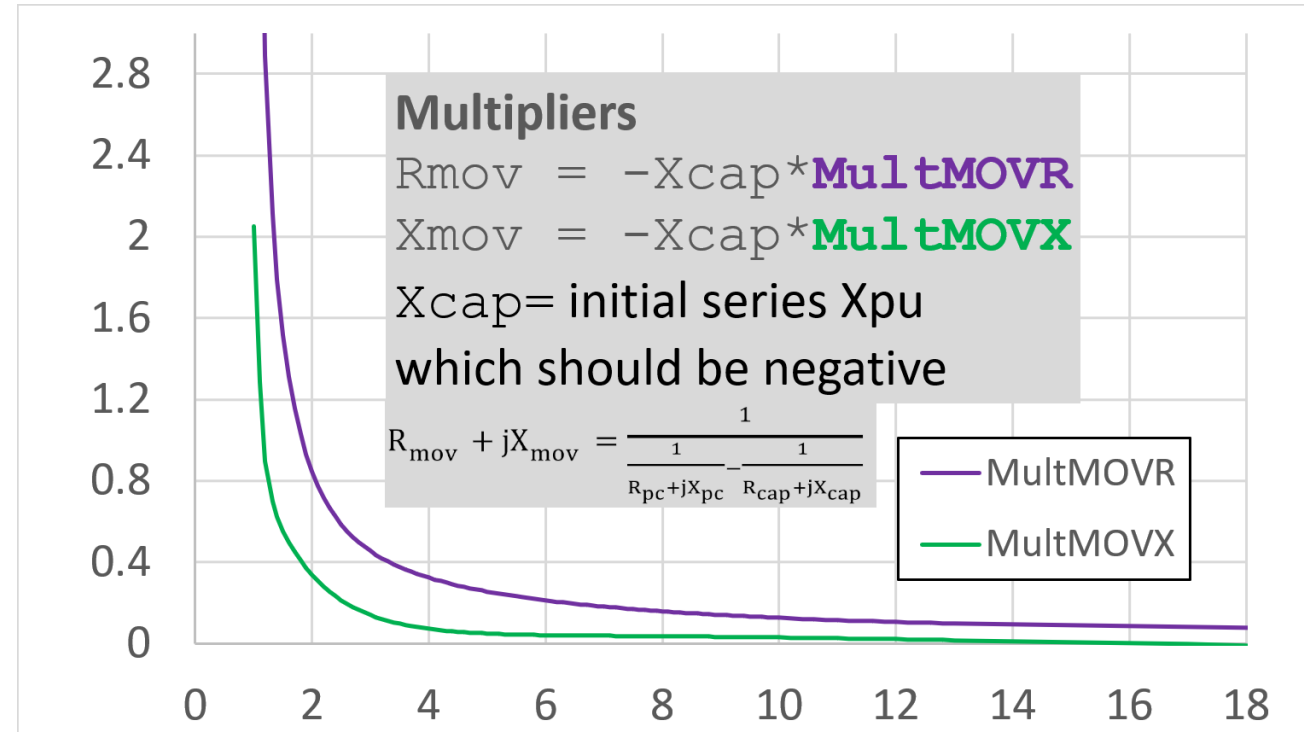


Graph of the $R_{mov} + jX_{mov}$



- Previous Graph was for Equivalent Impedance of the CAP+MOV
 - We can calculate the MOV impedance using equation
- Near value of $I_{pux} = 0.94879$ the impedance goes towards infinite
- As I_{pux} increases the impedance gets smaller and smaller
 - Eventually the SCMOV model will bypass it

$$R_{mov} + jX_{mov} = \frac{1}{\frac{1}{R_{pc} + jX_{pc}} - \frac{1}{R_{cap} + jX_{cap}}}$$



Input Parameters



- **Icrated**
 - Current Base in Amps for the mode
- **Icappro**
 - Used in Ipux calculation
- **Ithresh**
 - Value of Ipux at which we assume the MOV begins conducting
 - PowerWorld requires that Ithresh ≥ 0.94879
- All other values are used in transitions between the 3 modes of operationing

Icrated	Capacitor Rated current in Amps
Icappro	Capacitor protective level current, pu on Icrated base
Ithresh	Threshold value for MOV activation. Any value smaller than 0.94879 will be ignored and treated as equal to 0.94879.
Enerlim	MOV energy limit in Mjoules
Enerdly	Bypass delay associated with Enerlim in seconds
Imovlim	MOV current limit in pu of Icrated
Imovdly	Bypass delay associated with Imovlim in seconds
Icaplim	Capacitor current limit in pu of Icrated
Icapdly	Bypass delay associated with Icaplim in seconds
Iinsert	Insertion current in pu of Icrated
Tinsert	Insertion time in seconds

NORMAL (Mode 0)



- The original Rpu and Xpu of the series capacitor is used
- Currents used in reporting and mode transitions
 - I_{tot} = magnitude of current through the branch
 - $I_{cap} = I_{tot}$
 - $I_{mov} = 0$

CAP+MOV (Mode 1)



- The $R_{pc} + jX_{pc}$ is calculated (see earlier multipliers)
- Also, while operating in this mode, the energy absorbed by the MOV is calculated by using the resistance of the equivalent impedance $R_{pc} + jX_{pc}$ and the $R_{cap} + jX_{cap}$

$$R_{mov} + jX_{mov} = \frac{1}{\frac{1}{R_{pc} + jX_{pc}} + \frac{1}{R_{cap} + jX_{cap}}}$$

- The power absorbed over a time step is the resistive loss calculated as

$$\text{MegaWattMOV} = (R_{mov} * I_{movpu} * I_{movpu}) * \text{SystemMVABase}$$
- Energy absorbed by MOV is integrated by accumulating using the function

$$\text{EnergyMOV} = \text{EnergyMOV} + \text{MegaWattMOV} * \text{TimeStep}$$
- Currents used in reporting and mode transitions
 - I_{tot} = magnitude of current through the branch
 - I_{cap} = current calculated from terminal voltage and original $R_{cap} + jX_{cap}$
 - I_{mov} = magnitude of complex current calculation ($I_{tot} - I_{cap}$)

BYPASS (Mode 2)

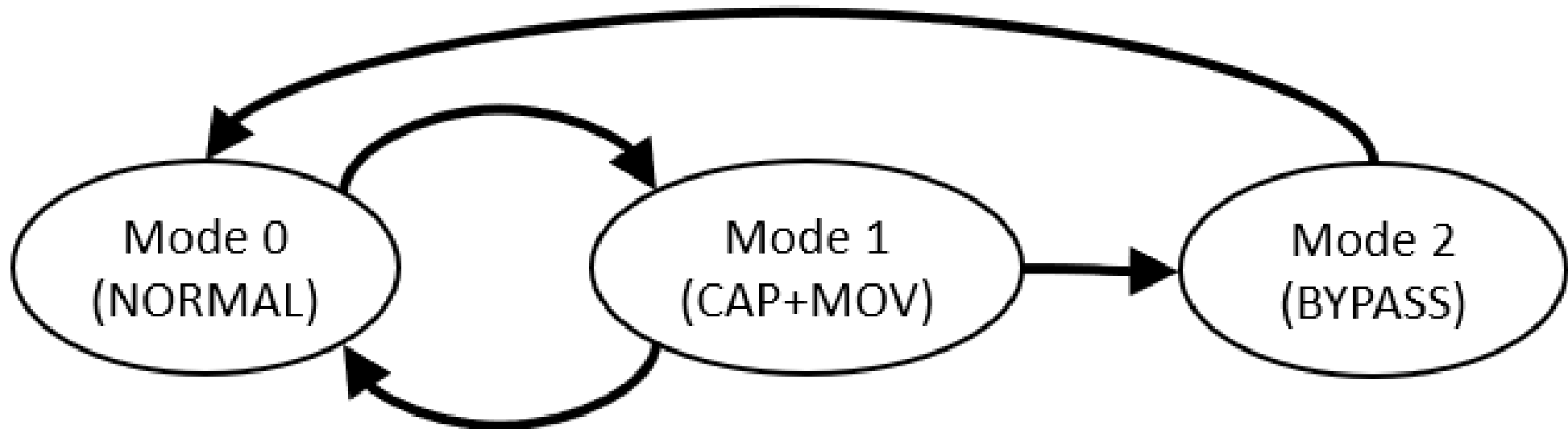


- When a decision to bypass the capacitor and the MOV, then the impedance is replaced by the very small impedance $0.00000001 + j0.000001$
- Currents used in reporting and mode transitions
 - I_{tot} = magnitude of current through the branch
 - $I_{cap} = 0$
 - $I_{mov} = 0$

Mode Transitions



- Direct transition from NORMAL to BYPASS is not allowed
- Direct transition from BYPASS to CAP+MOV is not allowed



Mode Transition

NORMAL (Mode 0) to CAP+MOV (Mode 1)



- When in Mode 0 (NORMAL), at the end of each time step of the simulation if the following condition is met then the device will switch to Mode 1 (CAP+MOV)
- $I_{pux} > I_{thresh}$, where $I_{pux} = I_{totAmp} / (I_{cappro} * I_{crated})$.
 - Note that the current base for getting I_{pux} in per unit is different than the per unit for comparisons to I_{caplim} and I_{movlim} described later because the multiplier I_{cappro} is used with I_{pux} .

Mode Transition

CAP+MOV (Mode 1) to NORMAL (Mode 0)



- When in Mode 1 (CAP+MOV), at the end of each time step, if $I_{pux} \leq I_{thresh}$ then the device transitions to Mode 0 (NORMAL) at next time step.

Mode Transition

CAP+MOV (Mode 1) to BYPASS (Mode 2)



- When in Mode 1 (CAP+MOV), at the end of each time step, three different checks are done to determine if a transition to Mode 2 (BYPASS) is made.
 - **Enerlim** If the accumulated energy absorbed by the MOV stored in **EnergyMOV** exceeds the MOV energy limit **Enerlim** for more than **Enerdly** seconds, then the device will bypass. Ignore if **Enerlim** = 0.
 - **Imovlim**: If the current passing through the MOV exceeds **Imovlim**, the capacitor and MOV are bypassed after a delay of **Imovdly** seconds. Ignore If **Imovlim** = 0.
 - **Icaplim**: If the current passing through the capacitor exceeds **Icaplim**, the capacitor and MOV are bypassed after a delay of **Icapdly** seconds. Ignore if **Icaplim** = 0.

Mode Transition

BYPASS (Mode 2) to NORMAL (Mode 0)

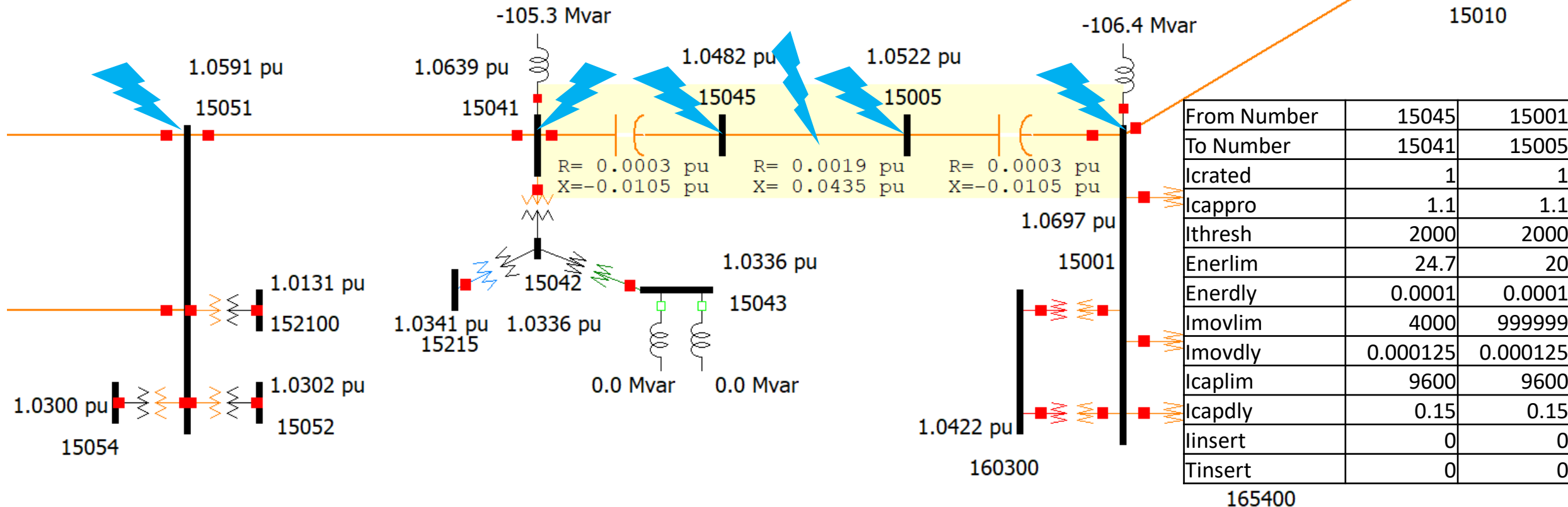


- When in Mode 2 (BYPASS), the model allows for reinsertion of the device if the bypass decision was made due to the **Imovlim** or the **Icaplim**. Reinsertion will occur if all other bypass conditions are not met and the current is below the **linsert** for **Tinsert** seconds.
- When this transition occurs the **Enerdly** timer for **Enerlim** is reset and will start counting again
- If the device was set to BYPASS due to the **EnerLim**, then the device will not reinsert the capacitor and MOV.
 - One exception to this is if another stability model or a user event has intentionally removed the Bypass, then this transition will reset the **EnergyMOV** = 0 and reset the **Enerdly** timer.
 - *** Should we do this? We will discuss this at the end of this presentation***

Large System Example from WECC



- Series caps on either end of branch from 15045 to 15005
- Study fault at the 7 lightning bolt locations

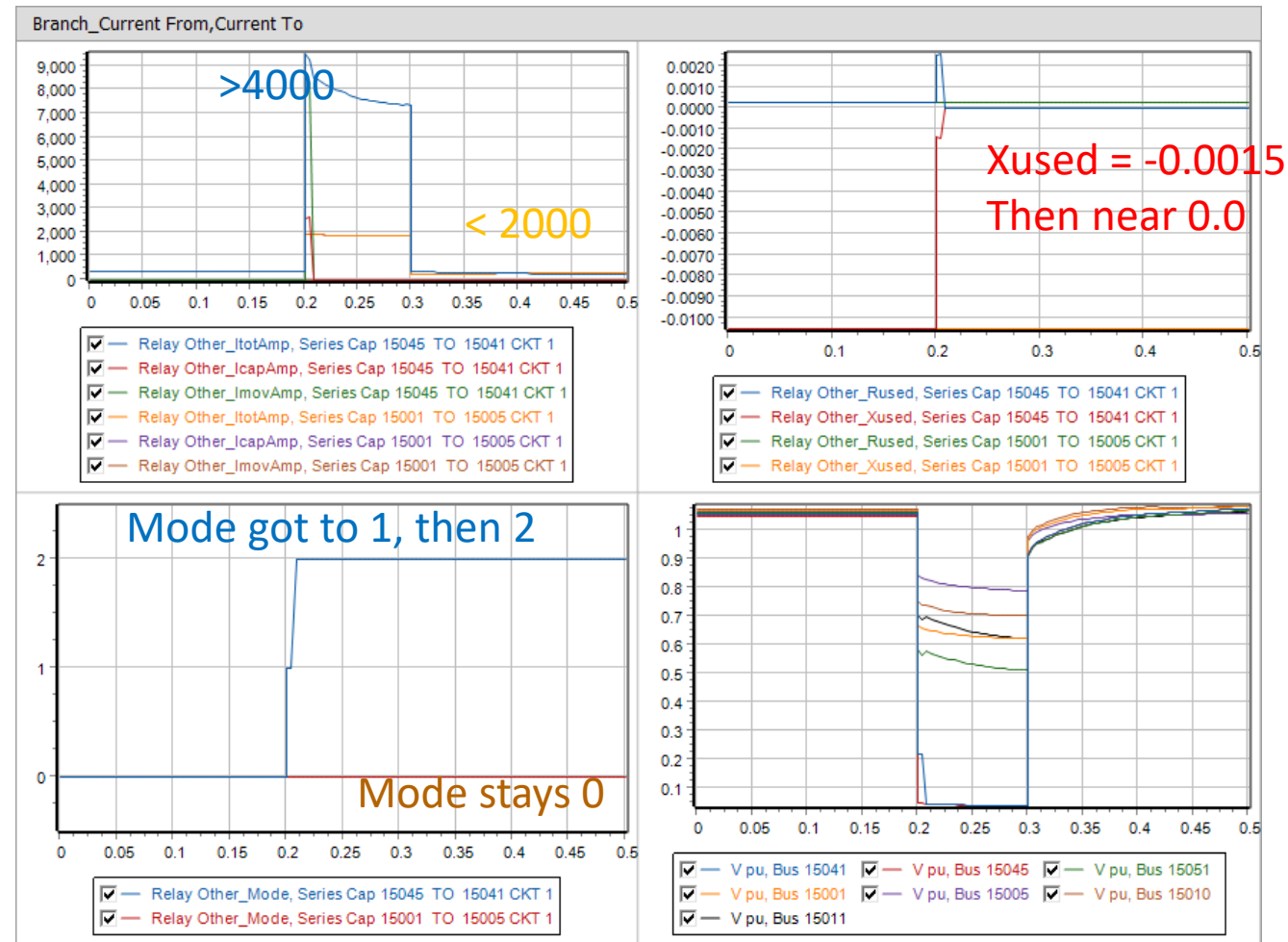


Example Simulation Result for Fault at 15045 (Line side terminal of Series Capacitor)

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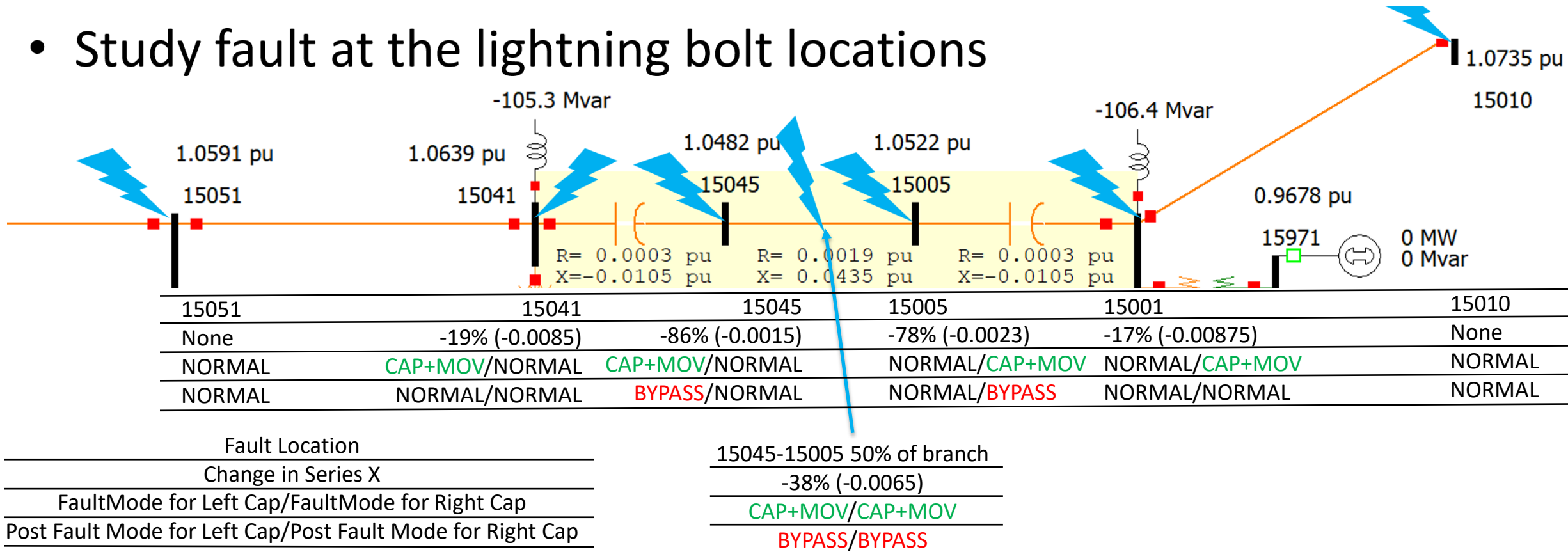
- Fault At Bus 15045
- 15045 – 15041
 - Current goes to above 9000 Amps
 - Mode = 1 (CAP+MOV)
 - Current is $> I_{movlim}$ (4000)
 - Go to Mode = 2 (BYPASS) quickly
- 15001 – 15005
 - Current stays below 2000 Amps
 - Mode = 0 (NORMAL) entire time



Used Input Parameters from Utility



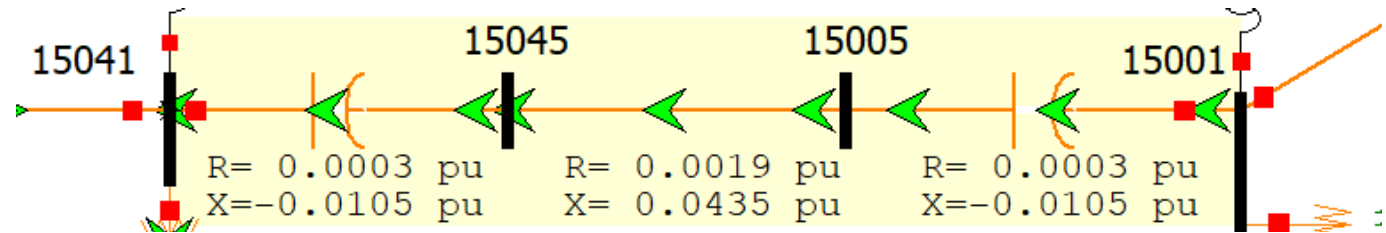
- Study fault at the lightning bolt locations



Summary



- Faulting anywhere except directly at terminals (15054 or 15010)
 - The SCMOV does nothing
- Faulting the system-side of the series caps (15041 or 15001)
 - Small (about 20%) impedance drop during the fault, immediately recovers after clearing
 - Only adjacent series cap responds, the other cap does not respond
 - This is close to having nothing happen
- Faulting the line-side of the series caps (15045 or 15005)
 - Large (about 80%) impedance drop on fault and then very quickly a bypass of device
 - Only adjacent series cap responds, the other cap does not respond
- Faulting in the middle of the branch from 15045 to 15005)
 - Medium (about 40%) impedance drop on fault and then very quickly a bypass of device
 - BOTH series cap respond this way



What did we learn from this example?

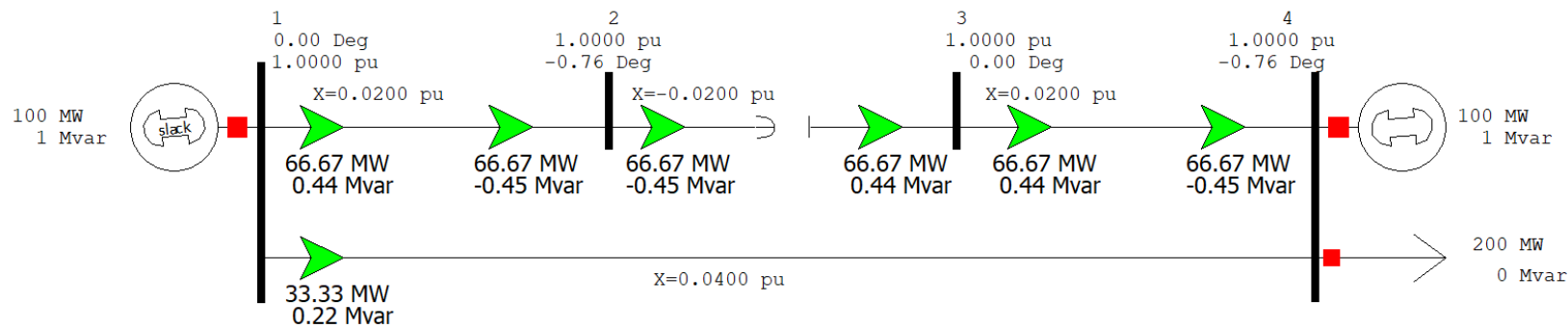


- SCMOV only responded to faults inside the network bounded by these example series capacitors
 - Properly functioning relays would trip all these devices for these faults
- This SCMOV is primarily important for a very specific study
 - Faults on the line-side of the series caps
 - Even then, if we assume the devices trip it will only change the behavior during the fault time, unless we assume primary protection fails
- This is a very localized and specific study

Small Test Example Simulation



- Following sample system has all 230 kV buses. All resistances are 0.0. Other information needed for network model is in picture.



- The Series Cap from bus 2-3 has the SCMOV parameters below. A constant impedance model is used for the load at bus 4.

Dynamic Model Parameters for Test System



- Generator MVABase for both generators is 500 MVA and the following GENROU Machine, ESAC1A Exciter and TGOV1 Governor models and parameters.

GENROU	
H	3
D	0
Ra	0
Xd	2.1
Xq	0.5
Xdp	0.2
Xqp	0.5
Xdpp	0.18
Xl	0.15
Tdop	7
Tqop	0.75
Tdopp	0.04
Tqopp	0.05
S1	0
S12	0
RComp	0
XComp	0

ESAC1A	
Tr	0
Tb	0
Tc	0
Ka	200
Ta	0.02
VaMax	7.5
VaMin	-7.5
Te	0.8
Kf	0.03
Tf	1
Kc	0.2
Kd	0.38
Ke	1
E1	3
SE1	0.03
E2	4
SE2	0.1
Vrmax	14
Vrmin	-14
Spdmlt	0

TGOV1	
Trate	0
R	0.05
T1	0.5
Vmax	1
Vmin	0
T2	2.5
T3	7.5
Dt	0

SCMOV	
Icrated	1000
Icappro	1
Ithresh	0.98
Deaccel	0.1
Enerlim	100
Enerdly	1
Imovlim	2
Imovdly	1
Icaplim	1.1
Icapdly	0.8
Operdly	0
linsert	0.3
Tinsert	2

$\text{Imovlim} * \text{Icrated} = 2000 \text{ Amps}$

$\text{Icaplim} * \text{Icrated} = 1100 \text{ Amps}$

$\text{linsert} * \text{Icrated} = 300 \text{ Amps}$

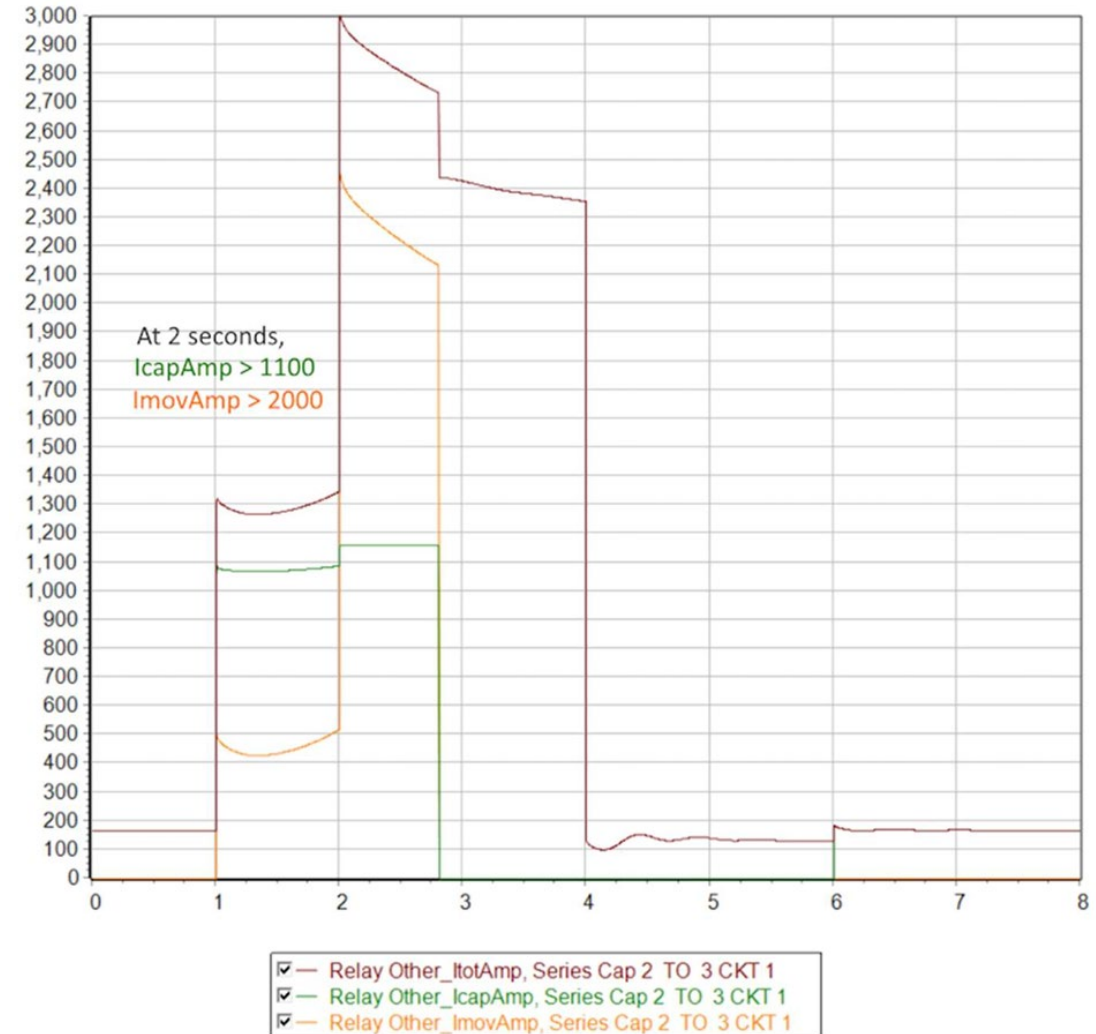
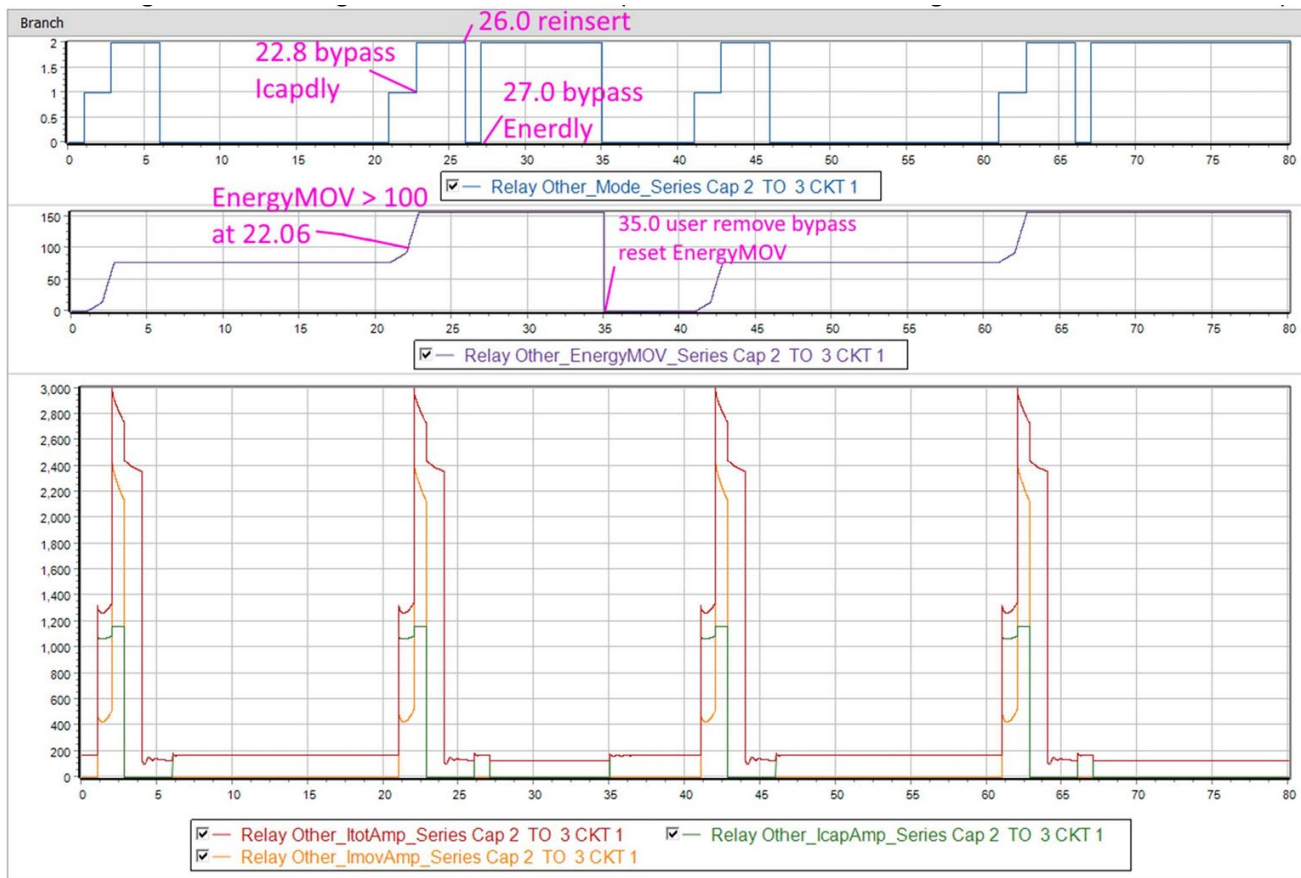
Example Simulation Run



- A Simulation is run that applies a fault at Bus 3 with fault impedance 0.1 per unit at 1.00 second. Fault impedance is changed to 0.02 at 2.00 seconds. Fault is cleared at 4.00 seconds. This sequence 3 events is then repeated at 20, 40, and 60 seconds. Finally, a user entered removal of the bypass is added at 35 seconds.

Time	Object	Action
1.0	Bus 3	FAULT 3PB IMP 0 0.1
2.0	Bus 3	FAULT 3PB IMP 0 0.02
4.0	Bus 3	CLEARFAULT
21.0	Bus 3	FAULT 3PB IMP 0 0.1
22.0	Bus 3	FAULT 3PB IMP 0 0.02
24.0	Bus 3	CLEARFAULT
35.0	Branch 2 3 1	NOTBYPASS
41.0	Bus 3	FAULT 3PB IMP 0 0.1
42.0	Bus 3	FAULT 3PB IMP 0 0.02
44.0	Bus 3	CLEARFAULT
61.0	Bus 3	FAULT 3PB IMP 0 0.1
62.0	Bus 3	FAULT 3PB IMP 0 0.02
64.0	Bus 3	CLEARFAULT

Example Simulation Results



Description of the First 35 seconds



- Simulation Start
 - At 1.0 seconds the fault is applied and the current immediately exceed the I_{thresh} value and we transition to CAP+MOV mode, but we do NOT exceed any of the values that would cause bypassing.
 - At 2.0 second the fault impedance decreases causing currents to increase. Immediately the I_{movlim} and the I_{caplim} thresholds are exceeded and bypass events are scheduled with a delay of 0.8 and 1.0 seconds.
 - At 2.8 seconds, the series cap is bypassed due to the 0.8 second time delay for I_{capdly} .
 - At 3.0 seconds, the 2nd bypass event from I_{movdly} is ignored because bypassing has already occurred.
 - At 4.0 seconds the fault clears and the total EnergyMOV accumulated by that point is 78 MJ **which is not enough to cause a permanent bypass**
 - At 4.0 seconds, the I_{totAmp} drops below I_{insert} and the timer for T_{insert} starts
 - At 6.0 seconds the T_{insert} timer expires and the series cap is reinserted
- This sequence of events is then repeated at time 21 seconds, however this time the EnergyMOV has continued to accumulate and will change the response
 - At 22.06 seconds the $EnergyMOV > Enerlim$ value and if it stayed there until 23.06 seconds it would have done a permanent bypass, however the model bypasses before this at 22.8 seconds due to the I_{capdly} again.
 - At 24.0 seconds the T_{insert} timer starts again and the device is inserted at 26.0 second
 - At 26.0 seconds **the $EnergyMOV > Enerlim$ still so the $Enerdly$ timer starts**
 - At 27.0 seconds the $Enerdly$ timer expires and a permanent bypass is done.

Now a model design question?



- Once EnergyMOV>Enerlim SCMOV bypasses the entire device
- The only way the bypass can be removed is if the user specifically tells the simulation to remove the bypass
- If the user chooses to remove the bypass, I suggest we should reset the EnergyMOV = 0.00 and reset the EnerDly timer