

Clarification on Proper Use of REPC_B model:

The Renewable Energy Modeling Working Group (REMWG)¹ of the WECC Modeling Validation Subcommittee² has been developing over the past ten years a series of modularized, standard and publicly available set of dynamic models for use in large system planning studies for the main forms of renewable energy systems (RES) [1]. Various model specification and guideline documents have been published by REMWG [2], [3], [4], [5], [6], [7]. As these models are being widely used in the planning studies, misunderstanding and misuse of REPC_B have been observed. REPC_B is a complex-plant controller to coordinate controls among multiple devices, primarily for modeling hybrid power plants that have multiple technology in the same plant, e.g. a combination of solar PV and battery energy storage facilities. The model can also be used to model RES that have multiple groupings of inverter-based generation (BR) that are modeled as a multiple aggregated units, but are all controlled by one centralized power plant controller (PPC). As the hybrid plants become more common and possibility the future of renewable energy development, the REPC_B model is being increasingly used. The intent of this paper is to clarify and promote proper use of the REPC_B model. The paper focuses on the use of REPC_B for hybrid plants. However, as stated above the REPC_B model can also be used to model the PPC for a plant with a single inverter-based resources (IBR) technology where multiple aggregated IBR unit models are used. All the concepts in the paper apply to both applications.

Figure 1 below shows the control block diagram for REPC_B model. The following features should be noted:

1. Pmax and Pmin are defined for the entire plant, which represents the contractual active power output range, which is equal to or smaller than the sum of individual inverter active power output range.
2. Qmax and Qmin are defined for the entire plant, which represents the plant-level reactive capability to be used under the steady-state and small disturbances, which is equal to or smaller than the sum of individual inverter reactive capability.
3. Plant controller active power reference P_{ext} is distributed to multiple generators by weighting factors of K_{zi} .
4. Plant controller reactive power/voltage reference W_{ext} is distributed to multiple generator by weighting factors of K_{wi} .

¹ Previously called the Renewable Energy Modeling Task Force

² Previously called the Modeling and Validation Working Group

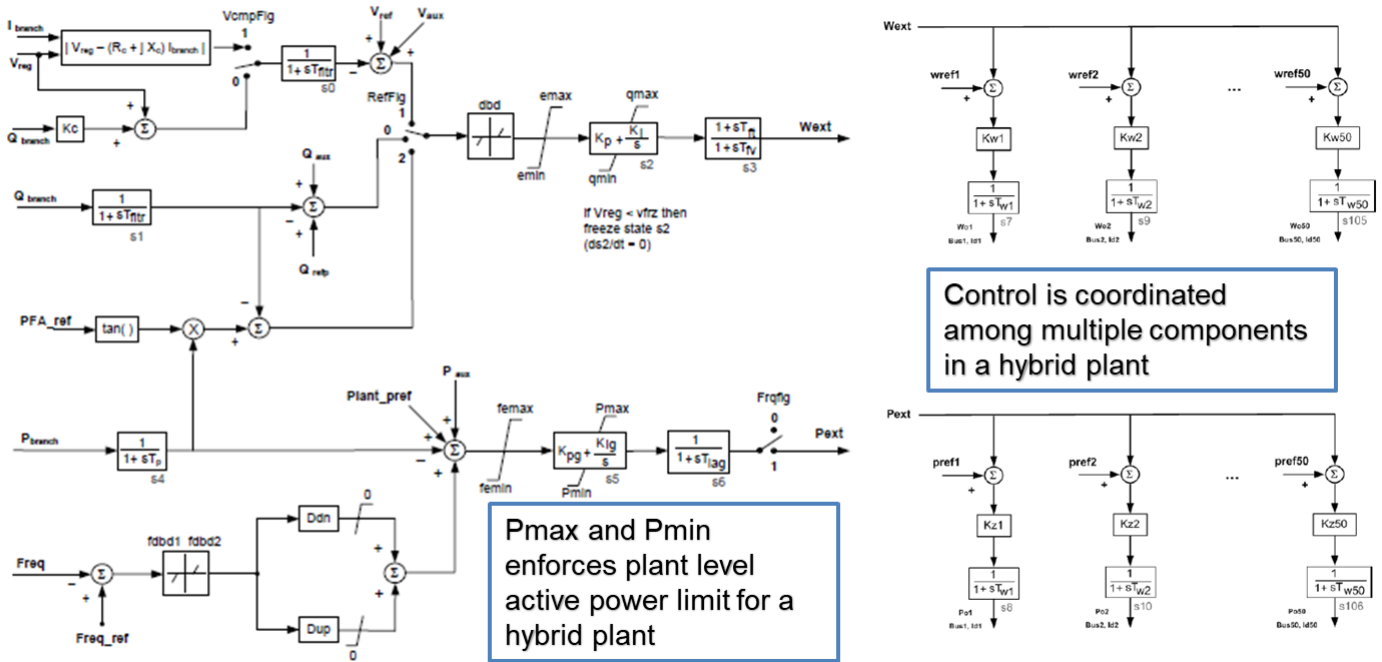


Figure 1: REPC_B control block diagram

In order to control multiple devices, the design of REPC_B is somewhat unique and different from the rest of the RES model suite. Special attention is needed when setting up the REPC_B model –

- In some software implementations, the model is always on the system MVA base. All the per unit parameters should be provided on the proper MVA base. In software packages where the model has its own MVA base, it is then preferable to use the MVA based of the entire plant.
- Pext and Wext initialize to 0. For this reason, all the control quantities are deviation from their initial values. Therefore, all the limits in the model are relative or deviation limits.
- Qmax and Qmin could be either reactive power deviation limits or voltage deviation limits depending on the configuration of the downstream REEC_* models of the controlled generators.
- The weighting factors Kzi and Kwi are not normalized by the software. The user must appropriately scale/normalize these per the MVA base on the downstream devices.
- The generator that REPC_B is attached to should be online. A monitor branch should be included in the REPC_B invocation. Note: in some software tools the model is a bus model (i.e. connected to a bus and not a generator). In these cases the invocation is not from a generator and so if any of the generators are out of service the status of the model is not affected.

Model MVA Base

Different software implement the REPC_B model differently. Some software provide an option to specify the model MVA base; some do not. Table 1 shows the major software implementation.



Table 1: REPC_B Implementation in Major Software

	Model Name	MVA Base
PSLF	REPC_B	System MVA base only
PSS/E	PLNTB	System MVA base or user specified model MVA base
PowerWorld	REPC_B	System MVA Base or user specified model MVA base (Supporting PSLF REPC_B and PSS/e PLNTB)
TSAT	REPC_B	System MVA Base or user specified model MVA base (Supporting PSLF REPC_B and PSS/e PLNTB)

When the model uses the system MVA base, all the parameters in per unit should be expressed on the system MVA base, i.e.

$$P_{max} = \frac{\text{Plant Maximum Output per Generation Interconnection Agreement}}{\text{System MVA Base}}$$

$$P_{min} = \frac{\text{Plant Minimum Output per Generation Interconnection Agreement}}{\text{System MVA Base}}$$

$$Q_{max} = \frac{\text{Plant Maximum Reactive Output under Steady State and Small Disturbance}}{\text{System MVA Base}} \quad (\text{See footnote}^3)$$

$$Q_{min} = \frac{\text{Plant Minimum Reactive Output under Steady State and Small Disturbance}}{\text{System MVA Base}} \quad (\text{See footnote}^3)$$

$$d_{up} = d_{dn} = \frac{1}{\text{droop}} \times \frac{\sum_{\text{all gens on REPC_B}} \text{Generator } P_{max}}{\text{system MVA base}}$$

Note: by Pmax in the above equation it is meant the nameplate rated MW capability of each generator.

Relative Limits

The reactive power command Wext and active power reference Pext initialize to 0. They are changes from the initial value. Therefore, pmax/pmin and qmax/qmin should be relative or deviation limits in per unit:

$$P_{max} = \text{Plant } P_{max} - \text{Initial } P_{gen}$$

$$P_{min} = \text{Plant } P_{min} - \text{Initial } P_{gen}$$

$$Q_{max} = \text{Plant } Q_{max} - \text{Initial } Q_{gen} \quad (\text{See footnote } 3)$$

$$Q_{min} = \text{Plant } Q_{min} - \text{Initial } Q_{gen} \quad (\text{See footnote } 3)$$

where Initial Pgen and Initial Qgen are the sum of the Pgen and Qgen of generators controlled by the REPC_B model.

³ The equations are applicable when Qmax and Qmin are reactive limits. See discussion later regarding reactive power or voltage limits.



These parameters depend on the generation dispatch, which is subject to changes in the planning studies and unknown to the Generator Owners who provide the models. To resolve this issue, the Generator Owners set the absolute limits in the model, i.e. as if initial P_{gen} and Q_{gen} are zero. The transmission planners will offset the limits by the initial conditions when performing planning studies⁴.

Reactive Power or Voltage Limits

The output W_{ext} could be either reactive power command or a voltage signal, depending on the electrical controller (REEC_*) models for the generators controlled by the REPC_B model. If the REEC models are in local voltage control mode ($pflag = 0$, $vflag = 0$, $qflag = 1$), W_{ext} is a voltage signal; otherwise, it is reactive power. This requires all the generators controlled by REPC_B take the same type of signal, voltage or reactive power. There should not be a mix of local voltage control mode with other voltage/reactive power control modes among the REEC models connecting to the same REPC_B model. When W_{ext} is voltage signal, Q_{max}/Q_{min} should be voltage deviation limits instead of reactive power deviation limits.

Kzi and Kwi

The software does not normalize the weighting factors K_{zi} and K_{wi} . It is up to the model users to set them up properly based on the control coordination in the actual power plant controller. Uncareful settings could cause unexpected results. For example, we have a power plant containing two generators that are 100MVA and 200MVA respectively and controlled by a REPC_B model on 100MVA base. Say we intend to control two generators real power output proportionally based on their generator size but set $kz1 = kz2 = 1$. When REPC_B model produces a command of $P_{ext} = 0.2$, it is meant to increase active output from the power plant by 20% of 100MVA, which is 20MW. But with $kz1 = kz2 = 1$, we get 40MW total output increase from the power plant, with the first generator providing 20% of its capacity (20MW out of 100MVA) and the second generator only contributed 10% of its capacity (20MW out of 200MVA). Another scenario is that one or more generators controlled by REPC_B are dispatched offline in a planning study. The K_{zi} and K_{wi} are not normalized among the online generators which could introduce inaccuracy.

Model Invocation

REPC_B model is attached to a generator in some software (PSLF, TSAT™, PowerWorld) and to a bus in others (PSS®E). In the case of it being attached to a generator, that generator must be online in the power flow model; otherwise the REPC_B model is turned off and not used. There is no good solution for this yet. The planners performing studies need to either keep the generator online even at zero MW output or modify the dynamic model to invoke the REPC_B from a different online generator. A dummy

⁴ Each software has its way of automating this. In case of PSLF platform, it can be done through a pre-run epcl in each of the transient simulation run. The pre-run epcl calculates the initial total P_{gen} and Q_{gen} and subtracts the initial values from the P_{max}/P_{min} and Q_{max}/Q_{min} in REPC_B models.



generator with zero MW and MVAR capability and always on may be added in each plant to attach the REPC_B model. Another key point about REPC_B invocation is that it should always include the monitored branch. Although REPC_B could still run without a monitored branch, it is inaccurate and incorrect, especially for hybrid plants that have plant level output limits and provide the frequency response.

Conclusion

As the only available power plant controller model for AC-coupled hybrid plants, REPC_B will see increased use in the near future. There are some inherent limitations that require more diligence to parameterize the models correctly and use the models properly in the planning studies. REMWG continues working on model enhancement to improve the model robustness and usability. A new power plant controller mode REPC_D will be developed and anticipated to replace REPC_B in the future. It should be based on the newly developed REPC_C model and expanded to allow it to connect to multiple downstream models like REPC_B, but resolve the limitations mentioned above of REPC_B.

References:

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